

PORTFOLIO
(2022 - 2024)

Presented by

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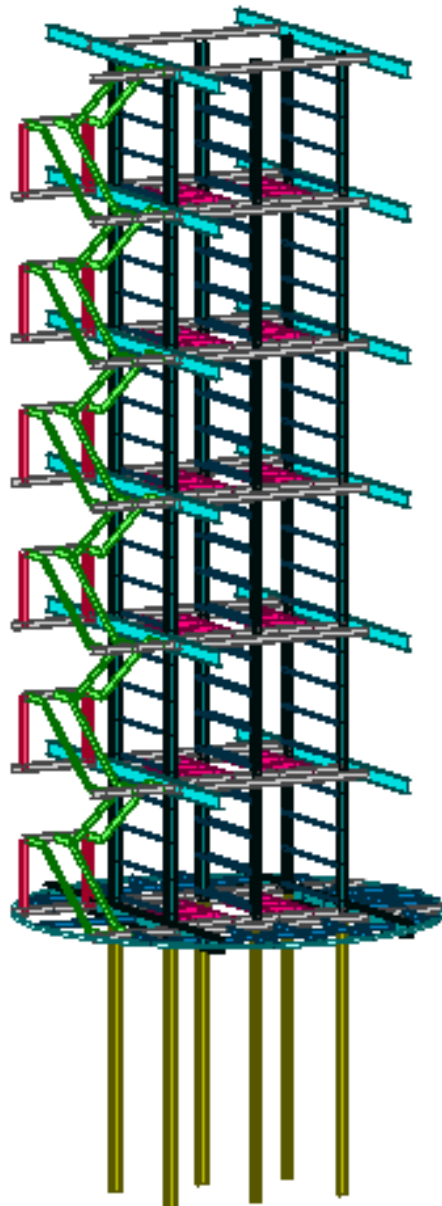
Project : Underground Cable Tunnel Construction Under Chao Phraya River
Company : Nawarat Patanakarn Public Company Limited
Title : Design Steel Platform (include checkered plate, grating slab and stairway)

The purpose of this project is to design steel member, steel connection, checkered plate, grating slab and stairway that refer from ANSI/AISC and ACI standard design code.

The structure model is refer from the owner that will give general dimension, general steel member section and general specification.

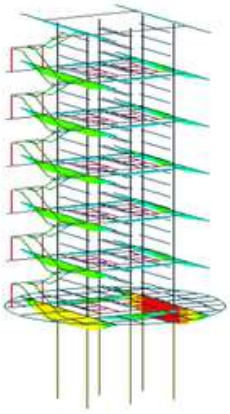
Procedure of this project is

1. Structure Analysis and Design by using Midas Gen
2. Steel Connection by using IDEA StatiCa
3. Checkered Plate and Grating Slab by using Microsoft Excel
4. Recheck result from Midas Gen and IDEAL Statica by using Microsoft Excel



Structure Model

Bending Moment Diagram (BMD)



MIDAS Gen
POST-PROCESSOR
BEAM DIAGRAM

MOMENT-y

27508.76
24885.92
22263.08
19640.24
17017.40
14394.56
11771.72
9148.88
6526.04
3903.20
0.00
-1342.48

CBALL: STL ENV-

MAX: 102
MIN: 493

UNIT: kgf*m

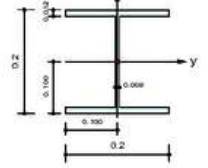
VIEW-DIRECTION
X: 0.483
Y: 0.857
Z: 0.259

Steel Checking Result

MIDAS	Company	Project Title
Author	USER	File Name
		D:_igned Load Platform\N.542.mgb

1. Design Information

Design Code: AISC-ASD89
 Unit System: kgf, m
 Member No: 135
 Material: SS400 (No:1)
 (Fy = 24000000, Es = 21000000000)
 Section Name: WF200x200 beam (No:3)
 (Rolled: H 200x200x8/12)
 Member Length: 5.86000



2. Member Forces

Axial Force: Fxk = 0.00000 (LCB: 1, POS:1/2)
 Bending Moments: My = 7039.12, Mz = 0.00000
 End Moments: Myl = 6237.02, Myr = 7039.12 (for Lb)
 Mj = -69.302, Mjr = -160.97 (for Lz)
 Mzl = 0.00000, Mzr = 0.00000 (for Lz)
 Shear Forces: Fyy = 0.00000 (LCB: 1, POS:1/2)
 Fzz = 4171.34 (LCB: 1, POS:J)

Depth	0.20000	Web Thick	0.00800
Top F Width	0.20000	Top F Thick	0.01200
Bot F Width	0.20000	Bot F Thick	0.01200
Area	0.00635	Asz	0.00160
Qyb	0.03207	Qzb	0.00500
Iyy	0.00005	Izz	0.00002
Ybar	0.10000	Zbar	0.10000
Syy	0.00047	Szz	0.00016
ry	0.06820	rz	0.05020

3. Design Parameters

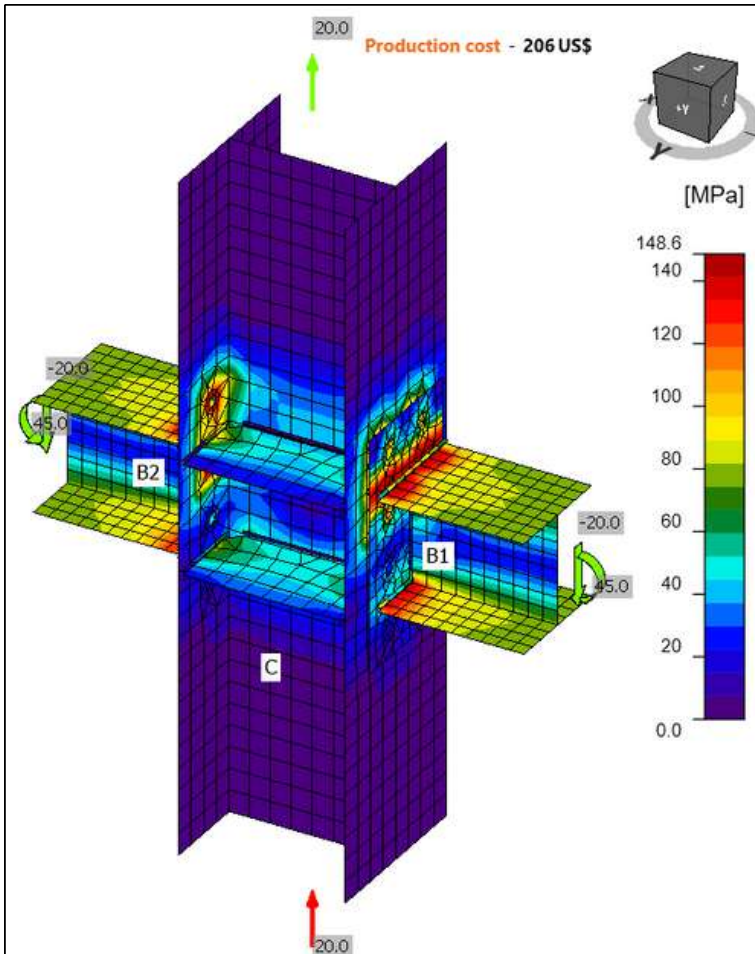
Unbraced Lengths: Ly = 5.86000, Lz = 1.46500, Lb = 1.46500
 Effective Length Factors: Ky = 1.00, Kz = 1.00
 Moment Factor / Bending Coefficient: Cm1 = 1.00, Cm2 = 1.00, Cb = 1.00

4. Checking Results

Slenderness Ratio: L/r = 116.7 < 300.0 (Memb:204, LCB: 1) O.K
 Axial Stress: f_t/F_t = 0/12000000 = 0.000 < 1.000 O.K
 Bending Stresses: f_{by}/F_{by} = 14913382/15840000 = 0.942 < 1.000 O.K
 f_{bz}/F_{bz} = 0/14400000 = 0.000 < 1.000 O.K
 Combined Stress (Tension+Bending): R_{max} = f_{bcy}/F_{bcy} + f_{bcz}/F_{bcz} = 0.942 < 1.000 O.K
 Shear Stresses: f_{vy}/F_{vy} = 0.000 < 1.000 O.K
 f_{vz}/F_{vz} = 0.272 < 1.000 O.K

Midas Gen Analysis

Midas Gen Result



IDEA StatiCa Analysis

Project: **โครงการก่อสร้างโรงโม่หินและโรงไฟฟ้าพลังแสงอาทิตย์พร้อมๆ กัน**
 Project no: **161 - นครราชสีมา**
 Author: **IDEA StatiCa**

Load effects (forces in equilibrium)

Name	Member	N [kN]	Vy [kN]	Vz [kN]	Mx [kNm]	My [kNm]	Mz [kNm]
LE1	C	20.0	0.0	0.0	0.0	0.0	0.0
	C	20.0	0.0	0.0	0.0	0.0	0.0
	B1	0.0	0.0	-20.0	0.0	45.0	0.0
	B2	0.0	0.0	-20.0	0.0	45.0	0.0

Check

Summary

Name	Value	Check status
Analysis	100.0%	OK
Plates	0.1 < 5.0%	OK
Bolts	70.4 < 100%	OK
Welds	75.1 < 100%	OK
Buckling	32.43	

Plates

Name	f _y [MPa]	Thickness [mm]	Loads	σ _{Ed} [MPa]	f _{pd} [%]	σ _{CEd} [MPa]	Check status
C-bf 1	248.2	15.0	LE1	148.8	0.1	22.4	OK
C-bf 1	248.2	15.0	LE1	148.8	0.1	22.4	OK
C-w 1	248.2	10.0	LE1	70.4	0.0	0.0	OK
B1-bf 1	248.2	12.0	LE1	148.8	0.0	0.0	OK
B1-bf 1	248.2	12.0	LE1	148.8	0.0	0.0	OK
B1-w 1	248.2	8.0	LE1	99.0	0.0	0.0	OK
B2-bf 1	248.2	12.0	LE1	148.8	0.0	0.0	OK
B2-bf 1	248.2	12.0	LE1	148.8	0.0	0.0	OK
B2-w 1	248.2	8.0	LE1	99.0	0.0	0.0	OK
EP1a	248.2	20.0	LE1	148.7	0.0	31.0	OK
EP1b	248.2	20.0	LE1	148.7	0.0	31.0	OK
STIFF1a	248.2	12.0	LE1	78.9	0.0	0.0	OK
STIFF1b	248.2	12.0	LE1	79.1	0.0	0.0	OK
STIFF1c	248.2	12.0	LE1	91.3	0.0	0.0	OK
STIFF1d	248.2	12.0	LE1	91.7	0.0	0.0	OK

Design data

Material	f _y [MPa]	f _{lim} [%]
A36	248.2	5.0

IDEA StatiCa Result

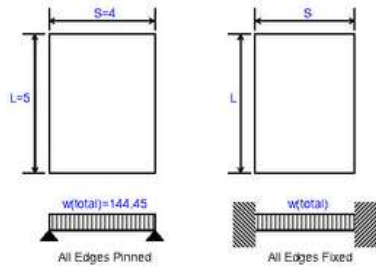
STEEL CHECKERED FLOOR PLATE DESIGN

For Rectangular Flat Plates Subjected to Uniformly Distributed Live Loading with Either All Edges Pinned or All Edges Fixed (per AISC 9th Edition ASD Manual)

Job Name:	อุโมงค์รถไฟใต้ดิน N.542 Tunnel Shaft B	Subject:	Checker Plate (Pin joint)
Job Number:		Originator:	Checker:

Input Data:

Long Span of Plate, L =	5.0000	ft.
Short Span of Plate, S =	4.0000	ft.
Plate Thickness, t =	1/2	in.
Uniform Live Load, w _L =	123.00	psf
All Edges Condition =	Pinned	
Yield Stress, F _y =	33.00	ksi
Allow. Deflection Ratio =	S/360	



Nomenclature for Rectangular Flat Plates

Results:

Flexural Stress:

Unif. Dead Load, w _{DL} =	21.45	psf
Unif. Load, w _{total} =	144.45	psf
f _{b(max)} =	3.80	ksi
F _{b(allow)} =	25.00	ksi

w_{DL} = floor plate self-weight in psf (per Reference #1)
 w_{total} = w_{DL} + w_L
 $f_b(max) = 0.75 \cdot (w_{total} / 144) \cdot (S^2 / 12) \cdot 2 / (t^3 \cdot (1 + 1.61 \cdot (S/L)^3)) / 1000$
 $F_b(allow) = 0.75 \cdot F_y$

f_{b(max)} <= F_{b(allow)}, O.K.

Deflection:

Aspect Ratio, α =	0.8000	
Mod. of Elasticity, E =	29000000	psi
Δ _(max) =	0.0980	in.
Δ _(ratio) =	S/490	
Allow. Δ _(ratio) =	S/360	

α = S/L
 E = 29,000,000 psi (assumed value for steel)
 $\Delta_{(max)} = 0.1422 \cdot (w_{total} / 144) \cdot (S^4 / 12) / (E \cdot t^3 \cdot (1 + 2.21 \cdot (S/L)^3))$
 $\Delta_{(ratio)} = (S^2 / 12) / \Delta_{(max)}$
 Allow. Δ_(ratio) = S/360 (user defined and selected)

S/490 <= S/360, O.K.

- References:**
- AISC Manual of Steel Construction (ASD) 9th Edition (Fourth Impression, 9/00), page 2-145.
 - "Design of Welded Structures", by Omer W. Biedgett (James F. Lincoln Arc Welding Foundation) Table 1, page 6.5-4 - taken from "Formulas for Stress and Strain" by Raymond J. Roark. These same formulas are found in "Design of Weldments" by Omer W. Biedgett (James F. Lincoln Arc Welding Foundation) in Table 1 on page 4.6-4.

Comments:

Steel Grating Design (G1)

1 Input Data

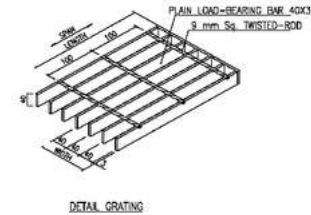
Req. Live Load =	600.00	kg/m ²
Clear Span =	1.10	m
Yielding Stress (F _y) =	2,400.00	kg/c
Allowable Stress (0.6F _y) =	1,440.00	kg/c
Grating Width =	3,340.00	mm
Grating Length =	1,100.00	mm
Impact Factor =	1.25	
Bar Thick. =	3.00	mm
Pitch of Load Bar =	40.00	mm
Flat Bar Height =	25.00	mm
Grating Weight =	0.59	kg/m

2 Design

Qty of Load Bar (N) =	84	ea.
Moment Required (M _r) =	120.92	kgm
Required Flatbar Height =	14.14	mm ok

3 Check

Section Modulus (S) =	312.50	mm ³
Allowable Stress (0.6F _y) =	1,440.00	kg/c
Moment Capacity (M _a) =	378.00	kgm
Moment ratio (M_r/M_a) =	0.32	<= 1.00 ok



DETAIL GRATING

Checked Plate Design

Grating Slab Design

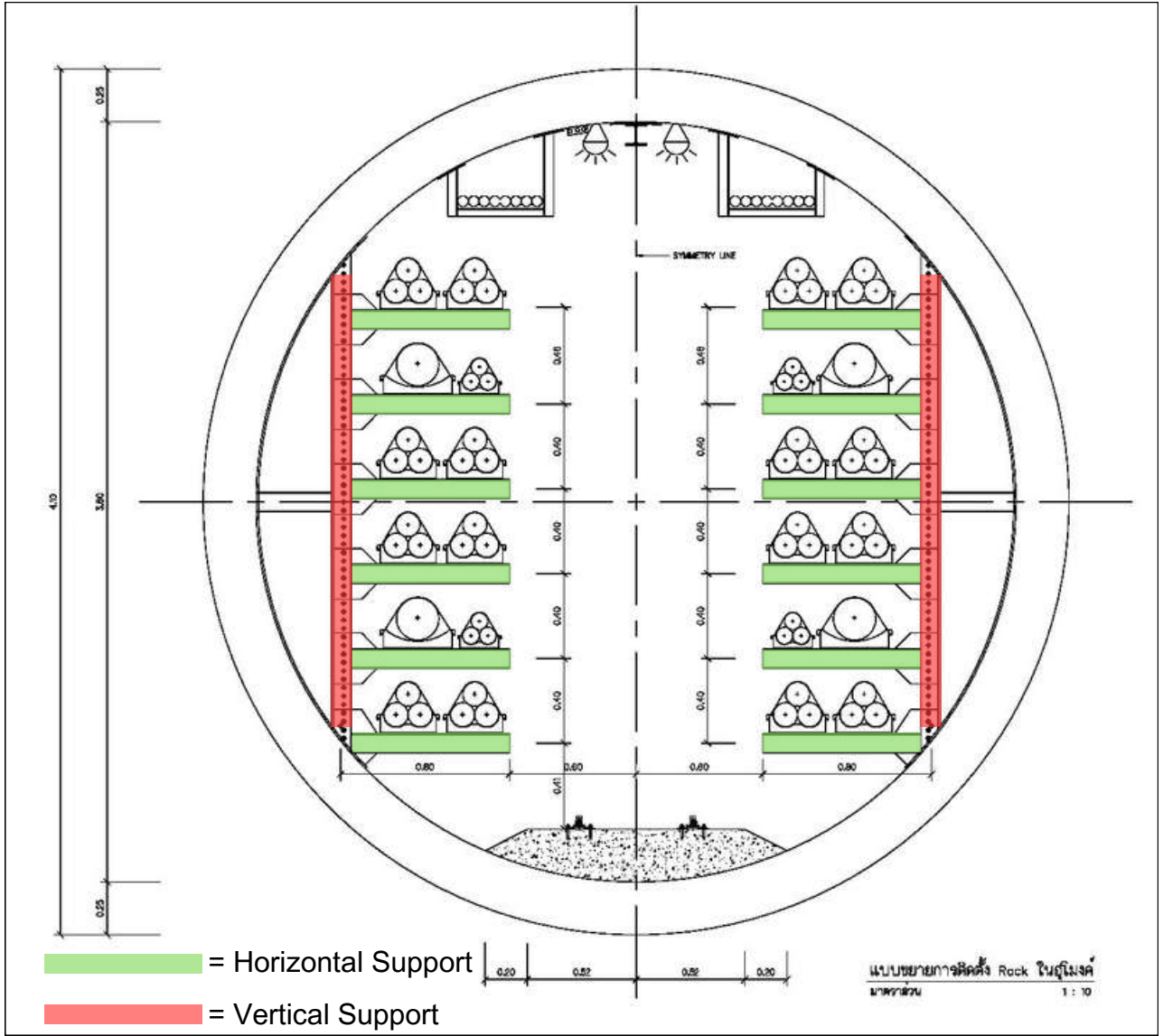
Project : Underground Cable Tunnel Construction Under Chao Phraya River
Company : Nawarat Patanakarn Public Company Limited
Title : Design Tunnel Cable Support

The purpose of this project is to design steel member (horizontal support and vertical support) and steel connection that refer from ANSI/AISC and ACI standard design code.

The structure model is refer from the owner that will give general dimension, general steel member section and general specification.

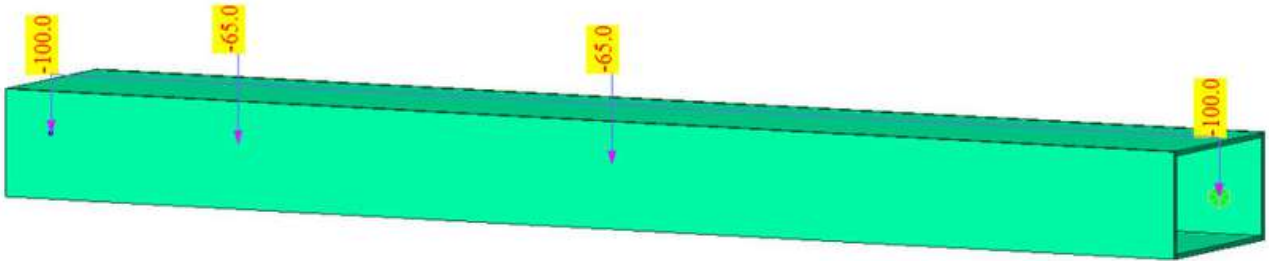
Procedure of this project is

1. Structure Analysis and Design by using Midas Gen
2. Steel Connection by using Microsoft Excel



Reference Drawing

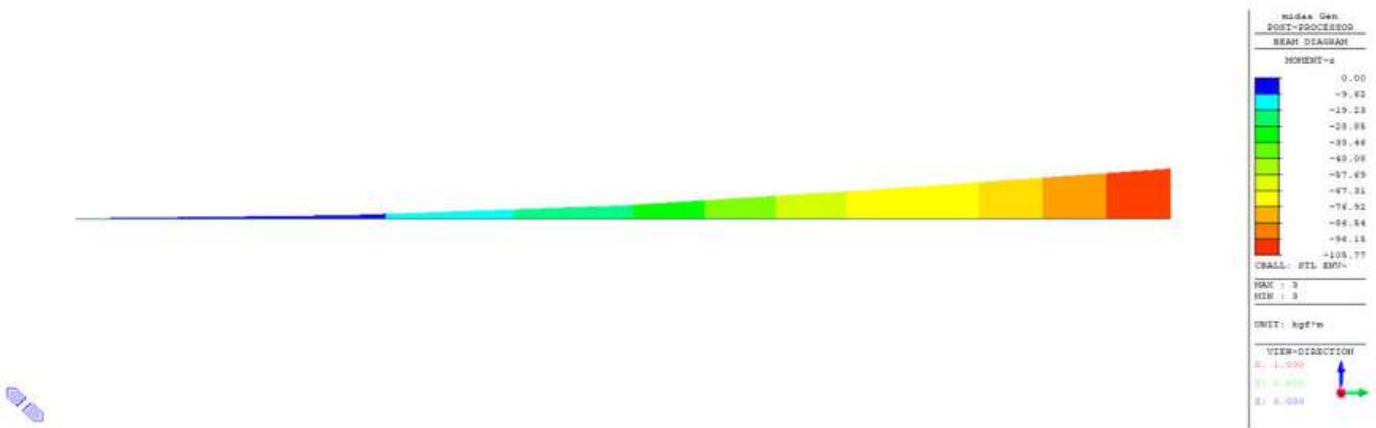
Analysis Section From Midas Gen



Element Load Assign

Horizontal Support Model

Analysis Section From Midas Gen



Bending Moment Diagram (BMD)

Midas Gen Analysis

Midas Gen		Steel Checking Result	
Company	Project Title	Author	File Name
MIDAS		USER	D:\L\Midas\Cable Support.mgb

1. Design Information

Design Code: AISC(15e)-ASD18
 Unit System: kgf, m
 Member No: 3
 Material: SS400 (No.1)
 (Fy = 240000.00, Es = 2100000000.00)
 Section Name: B 125x75x3.2 (No.1)
 (Rolled : B 125x75x3.2)
 Member Length : 0.80000

2. Member Forces

Axial Force: Fxk = 0.00000 (LCB: 2, POS:J)
 Bending Moments: My = 0.00000, Mz = -105.77
 End Moments: Myl = 0.00000, Myj = 0.00000 (for Lb)
 Myj = 0.00000, Myl = 0.00000 (for Ly)
 Mzl = 0.00000, Mzj = -105.77 (for Lz)
 Shear Forces: Fy = 133.809 (LCB: 3, POS:1/2)
 Fz = 0.00000 (LCB: 3, POS:1/2)

Depth	0.12500	Web Thick	0.00320
Flg Width	0.07500	Top Fl Thick	0.00320
Web Center	0.07150	Bot Fl Thick	0.00320

Area	0.00121	Asz	0.00050
Oyb	0.00404	Ozb	0.00293
Iyy	0.00000	Izz	0.00000
Iyy	0.03750	Zbar	0.00250
Iyy	0.00004	Szz	0.00003
Iy	0.04600	ry	0.03100

3. Design Parameters

Unbraced Lengths: Ly = 0.80000, Lz = 0.80000, Lb = 0.80000
 Effective Length Factors: Ky = 1.00, Kz = 1.00
 Moment Factor / Bending Coefficient: Cm1 = 1.00, Cm2 = 1.00, Cb = 1.00

4. Checking Results

Slenderness Ratio: L/r = 26.8 < 300.0 (Membr:3, LCB: 2) O.K
 Axial Strength: Pr/Pc = 0.017432, 3 = 0.000 < 1.000 O.K
 Bending Strength: Mry/Mcy = 0.000/743.533 = 0.000 < 1.000 O.K
 Mrz/Mcz = 105.767/488.618 = 0.228 < 1.000 O.K
 Combined Strength (Tension+Bending): Rmax = Pr/(2*Pc) + [Mry/Mcy + Mrz/Mcz] = 0.228 < 1.000 O.K
 Shear Strength: Vry/Vcy = 0.067 < 1.000 O.K
 Vrz/Vcz = 0.000 < 1.000 O.K

5. Deflection Checking Results

L/380.0 = 0.0022 > 0.0008 (Membr:3, LCB: 4, POS: 0.0m, Dir:Z) O.K

Modeling, Integrated Design & Analysis Software Print Date/Time : 09/26/2024 15:42

Midas Gen Result

DESIGN WELD CONNECTION FOR CANTILVER ARM, ASD2016

1. Data Criteria

1.1 Shear Force Required
 Shear Force Required (Va) = 220.00 kg

1.2 Material Property
 Steel
 Yielding Strength (Fy) = 2400.00 ksc
 Ultimate Strength (Fu) = 4000.00 ksc
 Elastic Modulus (Es) = 2,640,000.00 ksc

Weld
 Weld Grade = E60
 Ultimate Strength (Fexx) = 4,200.00 ksc

1.3 Cantilever Section Property
 Section: HSS125x75x3.2mm
 Weight (W) = 9.52 kg/m
 Depth (d) = 125.00 mm
 Width (bf) = 75.00 mm
 Web Thick (tw) = 3.20 mm
 Flange Thick (tf) = 3.20 mm

1.4 Plate Section Property
 Depth (dp) = 90.00 mm
 Width (bp) = 90.00 mm
 Thick (tp) = 3.20 mm
 d' = 50.00 mm
 b' = 50.00 mm

2. Determine Weld Connection

Shear Force Required (Va) = 220.00 kg
 Ultimate Strength (Fexx) = 4,200.00 ksc
 Safety Factor (Ω) = 2.00
 Weld Length (Le) = 9.00 cm
 Leg Size (tw) = 6.00 mm ok
 Allowable Shear Strength (Ra) = (0.6Fexx x 0.707 x Le x tw) / Ω = 4,810.43 kg
 Strength ratio = 0.05 < 1.00 ok

Steel Connection Calculation Sheet

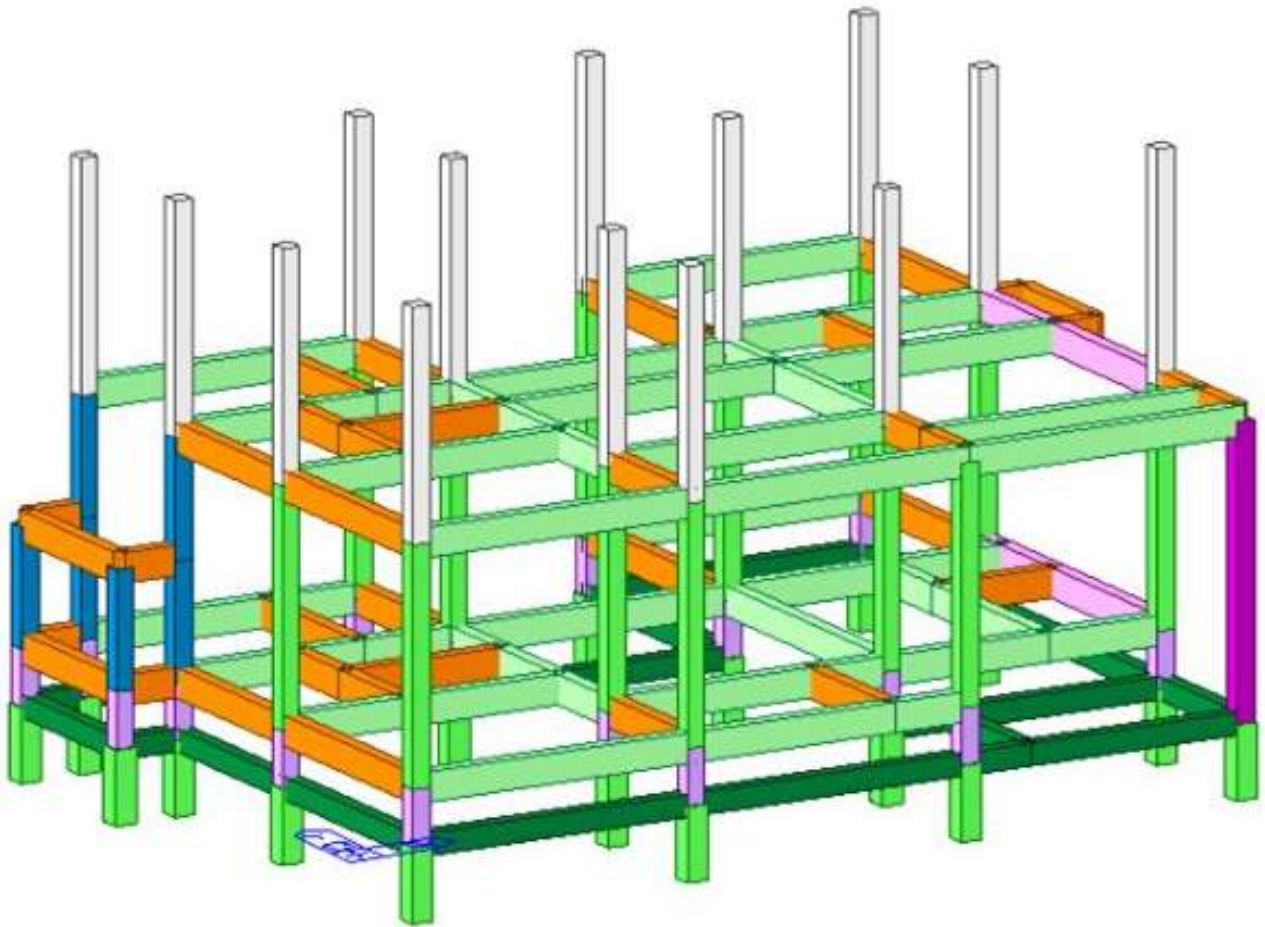
Project : 2 Floor Reinforced Concrete Residential House
Company : -
Title : Design Reinforced Concrete Structure

The purpose of this project is to design reinforced concrete beam, column, slab, stair and footing that refer from ACI standard design code.

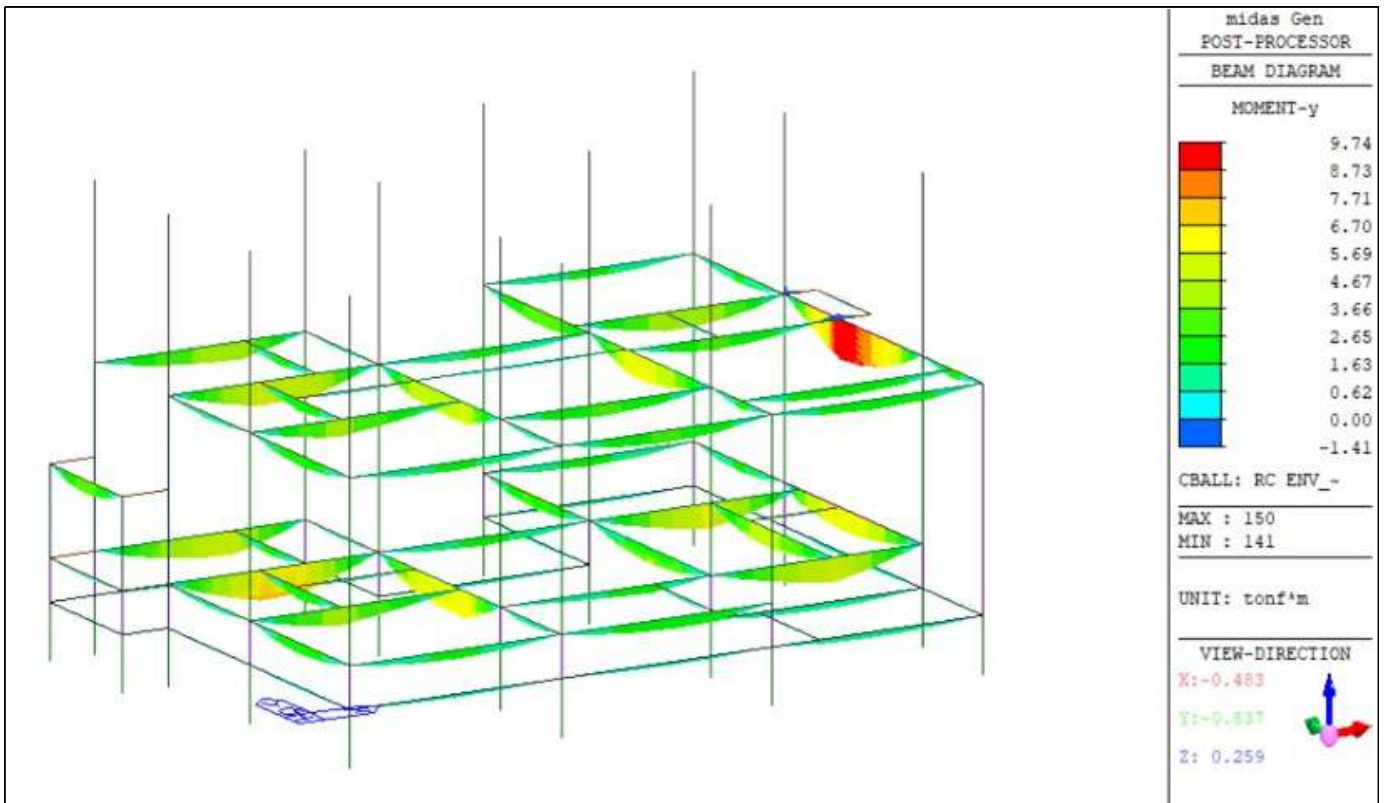
The structure model is refer from the owner that will give general dimension and requirements for section dimension.

Procedure of this project is

1. Structure Analysis by using Midas Gen
2. Beam and Column Design by using Midas Design+
3. Slab, Stair and Footing Design by Microsoft Excel



Structure Model



Midas Gen Analysis

■ MEMBER NAME : B1

1. General Information

Design Code	Unit System	Section	F_c	F_y	F_{st}
ACI318M-08	N,mm	200x400	23.54MPa	392MPa	235MPa

2. Forces and Reinforcement

SECT.	M_{top}	M_{bot}	V_o	Top Bar	Bot Bar	Stirrup
End(I)	9.463kN-m	42.35kN-m	62.21kN	2-P16	2-P16	2-P9@150
Middle	6.464kN-m	35.97kN-m	30.72kN	2-P16	3-P16	2-P9@150
End(J)	1.733kN-m	43.35kN-m	54.73kN	2-P16	2-P16	2-P9@150

3. Deflection

Support	Span	Short-term	Long-term	Duration
Case-1 (Pin-Pin)	3.500m	Span/360	Span/480	60 Months or more

$M_{s(l)}$	$M_{s(m)}$	$M_{s(j)}$	$M_{l(l)}$	$M_{l(m)}$	$M_{l(j)}$	M_{st}
0.000kN-m	22.16kN-m	0.000kN-m	0.000kN-m	6.129kN-m	0.000kN-m	100%

4. Check Bending Moment Capacity

SECT.	End(I)		Middle		End(J)	
	Top	Bot	Top	Bot	Top	Bot
POC.						

<http://www.midasuser.com>
 1/8

Midas Design+ Result

TWO WAY SLAB DESIGN USD METHOD Unit : MKS

PROJECT Didsaya House
DATE 4/8/2024

Step 1 Input Data Criteria

1.1 Load Required
 Dead Load (DL) = 2,400.00 kg/m³
 Super Dead Load (SDL) = 50.00 kg/m²
 Live Load (LL) = 200.00 kg/m²

1.2 Material Property
 Concrete
 Compressive Strength (f'c) = 240.00 ksc
 Elastic Modulus (Ec) = 233,928.00 ksc

Main Reinforcement
 Class = SD40
 Yielding Strength (Fy) = 4,000.00 ksc
 Ultimate Strength (Fu) = 5,700.00 ksc
 Elastic Modulus (Es) = 2,040,000.00 ksc

Stirrup Reinforcement
 Class = SR24
 Yielding Strength (Fy) = 2,400.00 ksc
 Ultimate Strength (Fu) = 3,900.00 ksc
 Elastic Modulus (Es) = 2,040,000.00 ksc

1.3 Slab Dimension
 Short Side (S) = 1.73 m
 Long Side (L) = 2.70 m
 S/L ratio = 0.64

Step 2 Determine Minimum Slab Thick.

Minimum Slab Thick. = (S + L) / 90 or 10.00 cm
 Provide Slab Thick. (h) = 10.00 cm or 10.00 cm
 Slab Self Weight Load (DL) = 240.00 kg/m²

Step 3 Determine Load Combination

Strength Load Case = 1.2DL + 1.6LL
 1.2DL + 1.6LL = 668.00 kg/m (consider per b = 1.00 m)
 Service Load Case = DL + LL
 DL + LL = 490.00 kg/m (consider per b = 1.00 m)

Step 4 Calculated Design Parameter

β_1 = 0.85
 Balanced As ratio (pb) = $\beta_1 \times (0.85F_c) / F_y \times 6120 / (6120 + F_y)$ = 0.0262
 Min.As ratio (pmin) = % Temp. Bar = 0.0018
 Max.As ratio (pmax) = 0.75pb = 0.0197
 Concrete Clear Cover (cc) = 2.00 cm
 Expect Rebar = DB12
 Effective Depth (d) = h - 2cc - 0.5db = 5.40 cm (short span)
 = h - 2cc - 1.5db = 4.20 cm (long span)

Slab Calculation Sheet

DESIGN บันไดห้องเริ่มพาดช่วงยาว USD METHOD Unit : MKS

PROJECT Didsaya House
DATE 4/8/2024

Step 1 Input Data Criteria

1.1 Load Required
 Dead Load (DL) = 2,400.00 kg/m³
 Super Dead Load (SDL) = 50.00 kg/m²
 Live Load (LL) = 200.00 kg/m²

1.2 Material Property
 Concrete
 Compressive Strength (f'c) = 240.00 ksc
 Elastic Modulus (Ec) = 233,928.00 ksc

Main Reinforcement
 Class = SD40
 Yielding Strength (Fy) = 4,000.00 ksc
 Ultimate Strength (Fu) = 5,700.00 ksc
 Elastic Modulus (Es) = 2,040,000.00 ksc

Temp. Reinforcement
 Class = SD40
 Yielding Strength (Fy) = 4,000.00 ksc
 Ultimate Strength (Fu) = 5,700.00 ksc
 Elastic Modulus (Es) = 2,040,000.00 ksc

1.3 Stair Dimension
 1st Floor Elevation = +0.75 m
 Landing Elevation = +2.35 m
 2nd Floor Elevation = +3.95 m
 Landing Length = 1.30 m

Step 2 Calculated Design Parameter

Trial Stair Step = 9 step
 Lower and Upper Elevation = 1.60 m
 Riser (R) = 17.78 cm
 Tread (T) = 25.00 cm + 2.50 cm (nosing)
 = 27.50 cm
 Horizontal Length (Lh) = $(0.25 \times 9) + 1.3$ = 3.55 m
 Assume Beam Width (b) = 20.00 cm
 Min. Stair Thick. = $(Lh + b) / 20$ = 18.75 cm
 Provide Stair Thick. (h) = 20.00 cm ok
 Stair Slab Load = $2400 \times h \times (\text{surf}(T^2 + R^2) / T)$ = 588.99 kg/m²
 Stair Step Load = $2400 \times 0.5 \times R$ = 213.34 kg/m²
 Stair Self Weight Load (DL) = 588.99 + 213.34 = 802.33 kg/m²

Step 3 Determine Load Combination

Strength Load Case = 1.2DL + 1.6LL
 1.2DL + 1.6LL = 1,342.80 kg/m (consider per b = 1.00 m)
 Service Load Case = DL + LL
 DL + LL = 1052.33 kg/m (consider per b = 1.00 m)

Stair Calculation Sheet

DESIGN SQUARE AND RECTANGULAR ISOLATED SPREAD FOOTING USD METHOD Unit : MKS

PROJECT Didsaya House
DATE 4/8/2024

Step 1 Input Data Criteria

1.1 Load Required
 Dead Load (DL) = 24.00 t
 Live Load (LL) = 5.00 t

1.2 Material Property
 Concrete
 Compressive Strength (f'c) = 240.00 ksc
 Elastic Modulus (Ec) = 233,928.00 ksc

Main Reinforcement
 Class = SD40
 Yielding Strength (Fy) = 4,000.00 ksc
 Ultimate Strength (Fu) = 5,700.00 ksc
 Elastic Modulus (Es) = 2,040,000.00 ksc

1.3 Soil Property
 Soil Type = ดินเหนียวหรือทรายปนเหนียว (พบบนดินดานและดินเหนียว พ.ศ.2522)
 Soil Unit Weight (γ) = 2.00 t/m³
 Bearing Capacity (qa) = 10.00 t/m²

Step 2 Determine Footing Dimension

Service Load (DL+LL) = 29.00 t
 Assume Wf = 10% x 29 = 2.90 t
 Design Load = DL + LL + Wf = 31.90 t
 Required Area of Footing = $(DL + LL + Wf) / qa$
 = 3.19 m²
 Provide Footing Width (B) = 1.80 m
 Footing Long (L) = 1.80 m
 Area of Footing (Af) = 3.24 m² >= 3.19 m² ok
 Trial Depth of Footing (h) = 30.00 cm
 Concrete Cover (cc) = 8.00 cm
 Effective Depth (d) = 22.00 cm >= 15.00 cm ok
 Footing Self Weight Load (Wf) = $2400 \times Af \times h$ = 2.33 t
 Soil Pressure (qu) = 9.67 t/m^2 <= 10.00 t/m² ok

Step 3 Determine Load Combination

Strength Load Case = $(1.2DL + 1.6LL) / Af$
 1.2DL + 1.6LL / Af = 11.36 t/m²

Step 4 Calculated Design Parameter

β_1 = 0.85
 Balanced As ratio (pb) = $\beta_1 \times (0.85F_c) / F_y \times 6120 / (6120 + F_y)$ = 0.0262
 Min.As ratio (pmin) = % Temp. Bar = 0.0018
 Max.As ratio (pmax) = 0.75pb = 0.0197

Isolated Footing Calculation Sheet

DESIGN COMBINED FOOTING USD METHOD Unit : MKS

PROJECT Didsaya House
DATE 4/14/2024

Step 1 Input Data Criteria

1.1 Load Required
 Pier A
 Dead Load (DL) = 15.00 t
 Live Load (LL) = 2.00 t
 Pier B
 Dead Load (DL) = 7.00 t
 Live Load (LL) = 1.00 t

1.2 Material Property
 Concrete
 Compressive Strength (f'c) = 240.00 ksc
 Elastic Modulus (Ec) = 233,928.00 ksc

Main Reinforcement
 Class = SD40
 Yielding Strength (Fy) = 4,000.00 ksc
 Ultimate Strength (Fu) = 5,700.00 ksc
 Elastic Modulus (Es) = 2,040,000.00 ksc

Temp. Reinforcement
 Class = SD40
 Yielding Strength (Fy) = 4,000.00 ksc
 Ultimate Strength (Fu) = 5,700.00 ksc
 Elastic Modulus (Es) = 2,040,000.00 ksc

1.3 Soil Property
 Soil Type = ดินเหนียวหรือทรายปนเหนียว (พบบนดินดานและดินเหนียว พ.ศ. 2522)
 Soil Unit Weight (γ) = 2.00 t/m³
 Bearing Capacity (qa) = 10.00 t/m²

1.4 Pier Dimension
 Pier A
 Pier Width (c1A) = 30.00 cm
 Pier Length (c2A) = 30.00 cm
 Pier B
 Pier Width (c1B) = 30.00 cm
 Pier Length (c2B) = 30.00 cm

Combined Footing Calculation Sheet

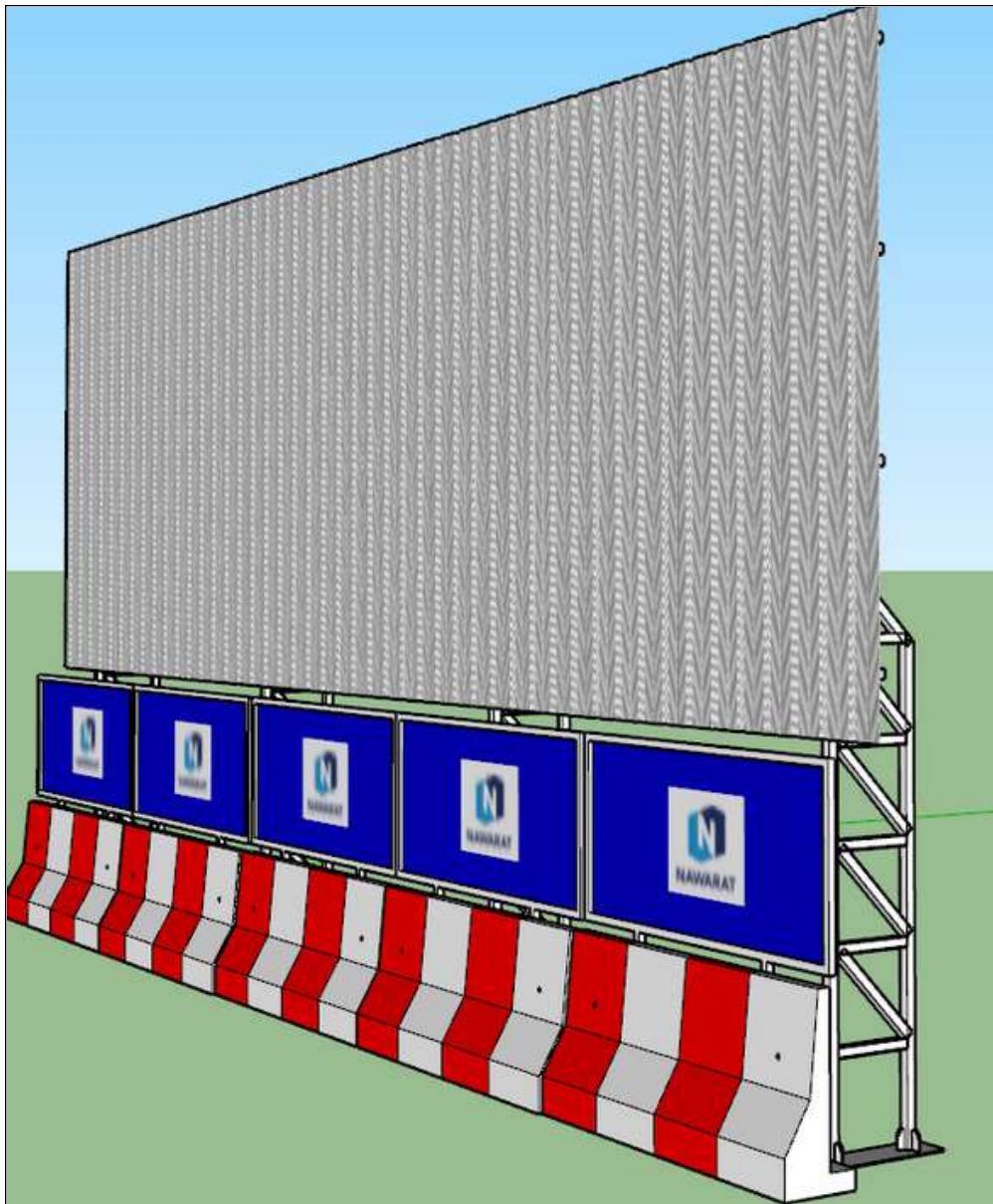
Project : The MRT Purple Line Project Contract 3 Underground Civil Works
Company : Nawarat Patanakarn Public Company Limited
Title : Design Steel Temporary Fence

The purpose of this project is to design steel temporary fence at the site location for protect public seeing the construction activity and equipment in work site that refer from ANSI/AISC and ACI standard design code.

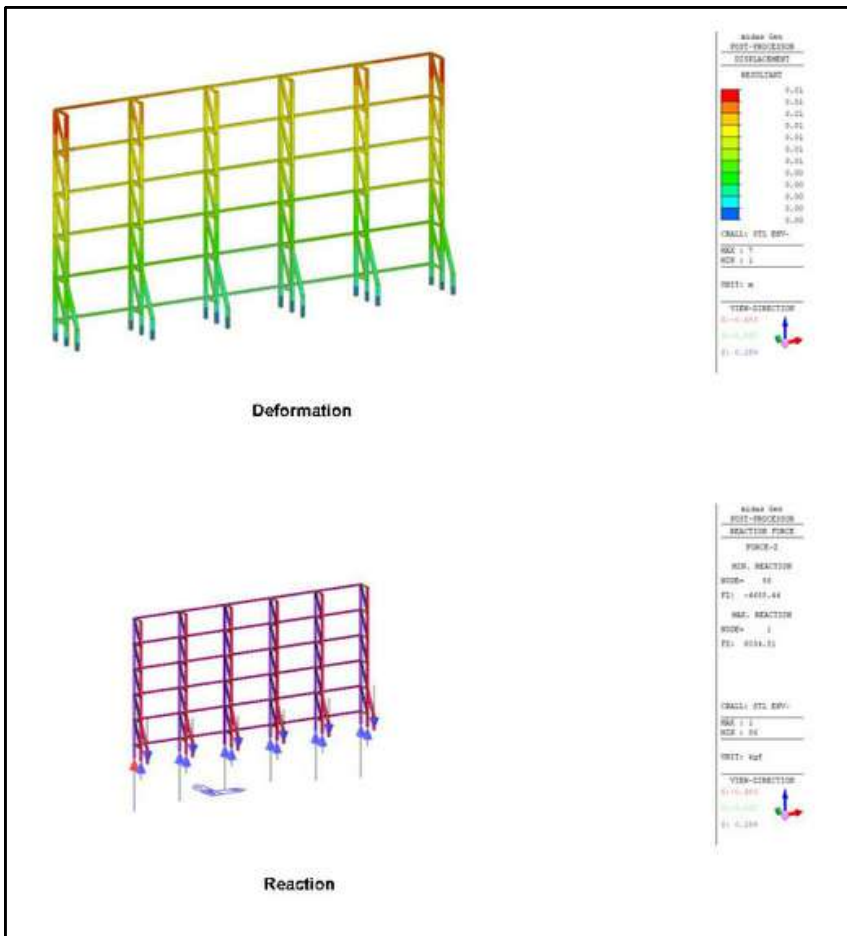
The structure model is refer from site requirements that will give general dimension.

Procedure of this project is

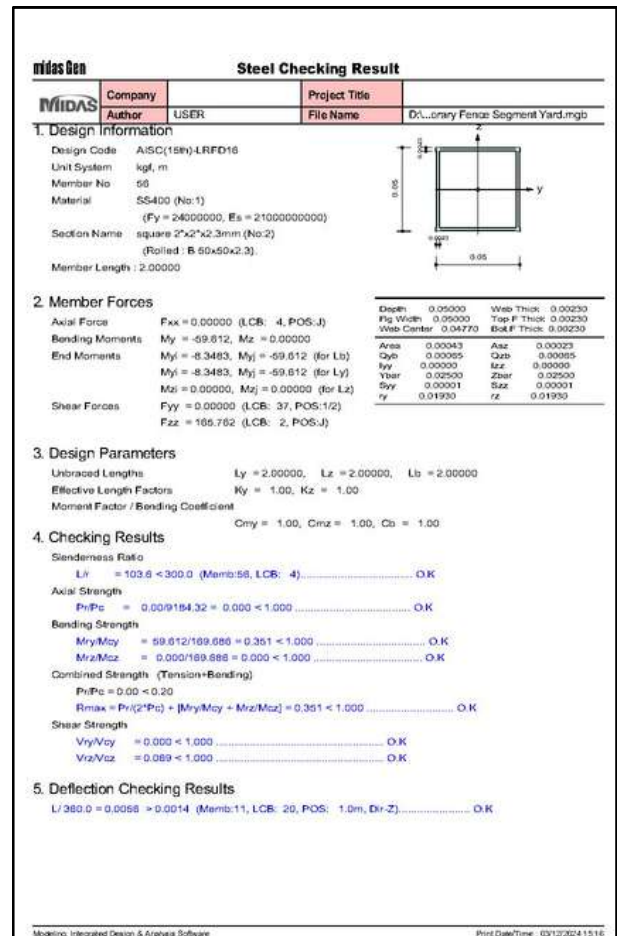
1. Structure Analysis and Design by using Midas Gen
2. Steel Connection by using IDEA StatiCa



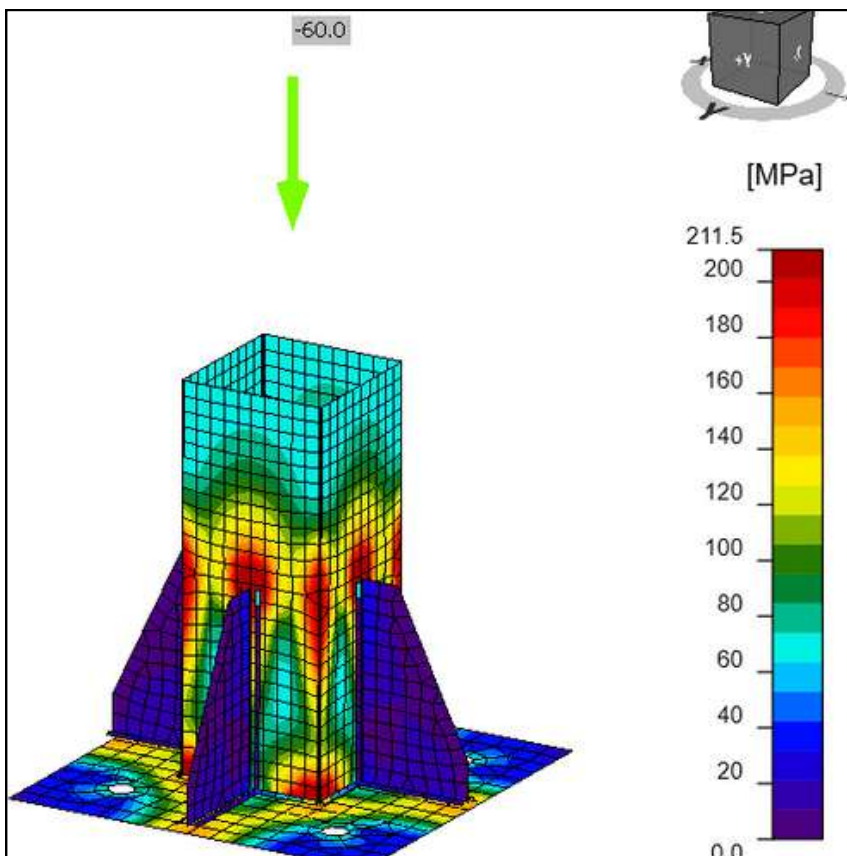
Site Requirement



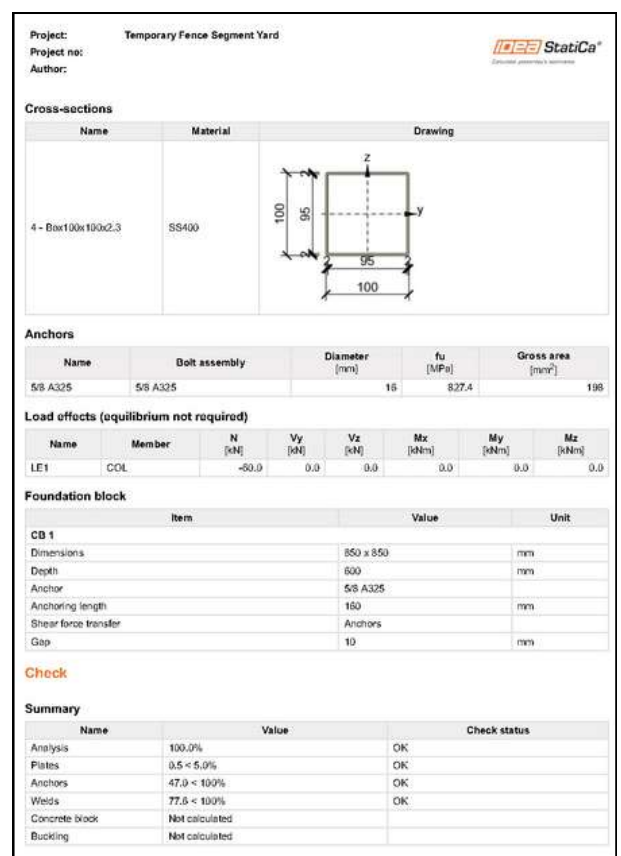
Midas Gen Analysis



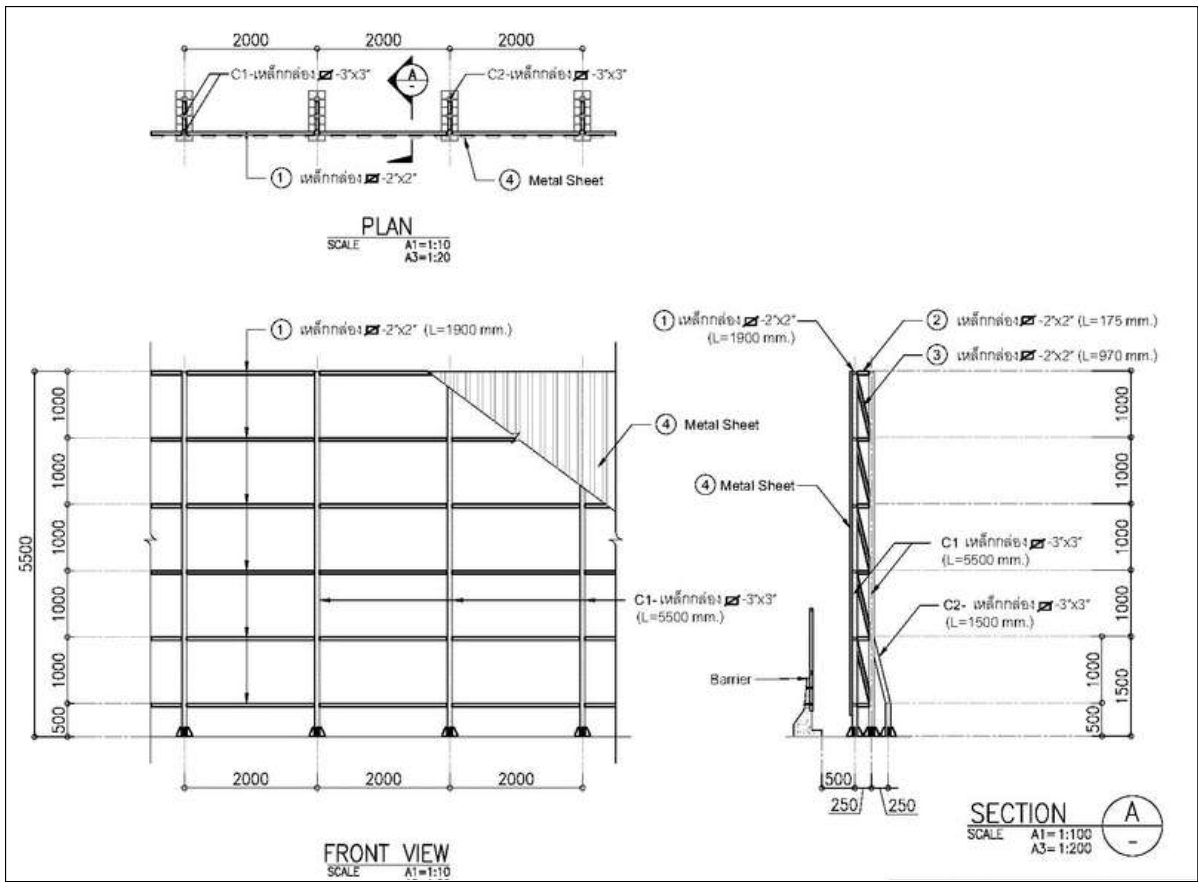
Midas Gen Result



IDEA StatiCa Analysis



IDEA StatiCa Result



Construction Drawing

Project : The MRT Purple Line Project Contract 3 Underground Civil Works
Company : Nawarat Patanakarn Public Company Limited
Title : Design Reinforced Concrete Beam for Support TBM

The purpose of this project is to design reinforced concrete beam for support TBM at site location that refer to ACI standard design code.

The structure dimension is refer from site requirements and Information for calculation is refer from TBM specification.

Procedure of this project is

1. Structure Analysis and Design by using Microsoft Excel

1/2

S/No	NAME	SKETCH	NUM	WEIGHT	NOTE
01	SHIELD BODY A-RING		1	90ton	INCLUDING
02	SHIELD BODY B,C,D-RING		1	95ton	INCLUDING
03	SHIELD BODY EF-RING (UPPER)		1	13ton	INCLUDING
04	SHIELD BODY EF-RING (LOWER)		1	13ton	INCLUDING
Maximum Weight for Design					
s.TOTAL				212ton	

2/2

S/No	NAME	SKETCH	NUM	WEIGHT	NOTE
05	CUTTER HEAD		1	40ton	INCLUDING
06	ERECTOR		1	16ton	INCLUDING
07	SCREW		1	17ton	INCLUDING
08	REAR SCAFFOLD		1	9ton	INCLUDING
09	MANLOCK		1	2.4ton	
s.TOTAL				84.4ton	
TOTAL				296.4+ ton	

TBM Specification

Structure Beam Type I

Requirement Load

Point Load, P	=	30.00 t	
Ultimate Point Load, Pu	=	42.00 t	(1.4Pd)
Span Length, L	=	1.65 m	
Max. Shear, Vmax	=	21.00 t	
Max. Moment, Mmax	=	8.66 tm	

ค่าคงที่สำหรับการออกแบบ

β_1	=	0.76	
Balanced Steel Ratio, ρ_b	=	0.03929	
Max. Steel Ratio, ρ_{max}	=	0.02947	
Min. Steel Ratio, ρ_{min}	=	0.00350	
Trial Ultimate Resistance, Ru	=	69.47 ksc	
ϕ moment	=	0.90	
ϕ shear	=	0.85	

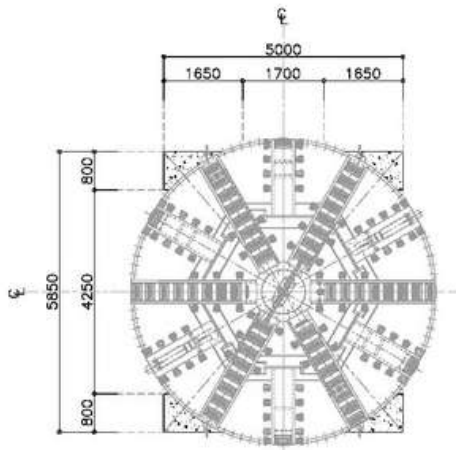
Required Section Area

Trial ρ	=	0.01964 (0.5 balanced)	
Trial Width, b	=	60.00 cm	
Effective Depth, d	=	13.16 cm	(distance from extreme compression to centroid rebar tension)
Choose d	=	54.00 cm	
assume d'	=	6.00 cm	(distance from extreme tension to centroid rebar tension)
Beam Type	=	general beam	
Depth, h	=	60.00 cm	ok
b x h	=	80 x 60 cm	

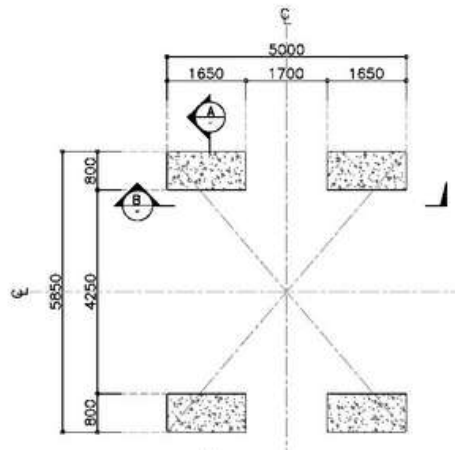
Design Longitudinal Reinforcement

Actual Ultimate Resistance, Ru	=	4.13 ksc	
Steel Ratio, ρ	=	0.00104	
Use Steel Ratio, ρ_{use}	=	0.00350 use min. % reinforced	
Rebar Required, As, req.	=	15.12 sq.cm.	
Choose Rebar	=	4 - DB25 1 layer	
Rebar Provided, As, prov.	=	19.63 sq.cm.	ok

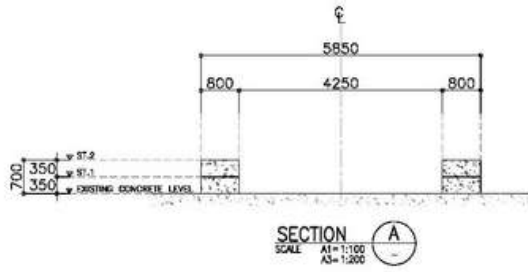
Calculation Sheet



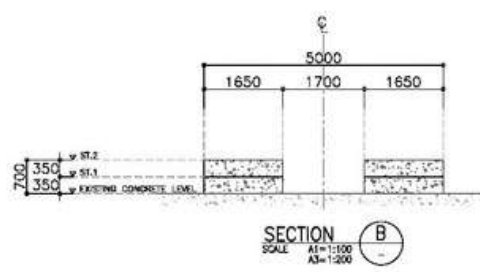
PLAN SUPPORT TBM CUTTER-HEAD
SCALE A1=1:100 A3=1:200



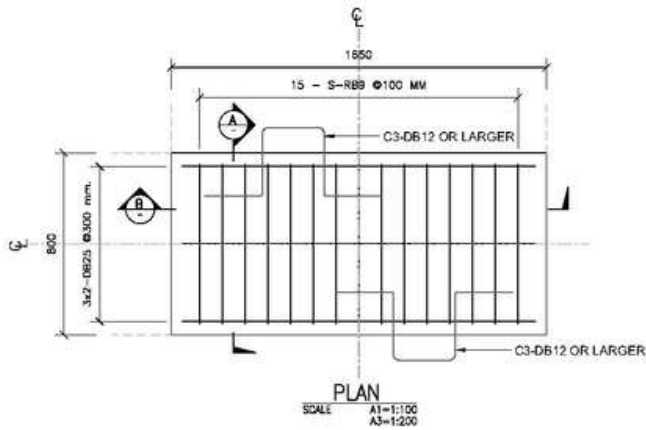
PLAN
SCALE A1=1:100 A3=1:200



SECTION A
SCALE A1=1:100 A3=1:200



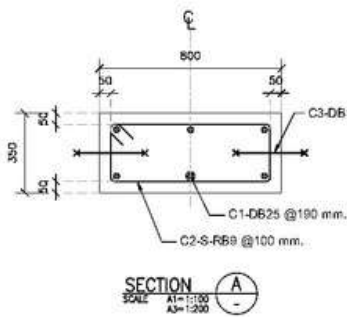
SECTION B
SCALE A1=1:100 A3=1:200



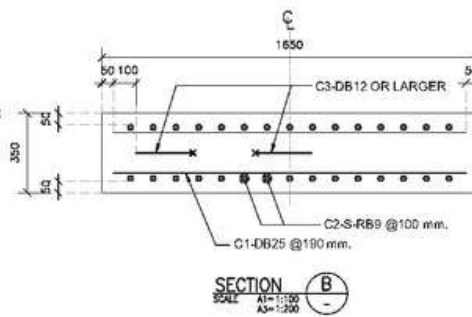
PLAN
SCALE A1=1:100 A3=1:200

BARBENDING FOR SUPPORT TBM

CODE	Dia	DIMENSION(mm)				RADIUS R	CUTTING LENGTH	NOG	SHAPE BAR
		A	B	C	D				
C1	DB25	1550					1550	6	
C2	RB9	700	250	150		17.5	2250	15	
C3	DB12	250	300			17.5	1350	2	



SECTION A
SCALE A1=1:100 A3=1:200



SECTION B
SCALE A1=1:100 A3=1:200

รายการประกอบแบบ
1 เสาเหล็ก
1.1 เสาเหล็ก มีหน้าตัดตามแปลนและมีเส้นผ่าศูนย์กลาง 100 มม. มีน้ำหนัก 20 กก. และมีรอยบากตามลักษณะ CUMBER #15300 ไร่.
2 เหล็กเสริมคอนกรีต
2.1 เหล็กกลม (ROUND BAR) ใช้เส้นผ่าศูนย์กลางมีขนาดตามตารางต่อไปนี้
GRADE SR 24 สลักเหล็กกลม ใช้เส้นผ่าศูนย์กลางมีขนาดตามตาราง และ GRADE SD 40

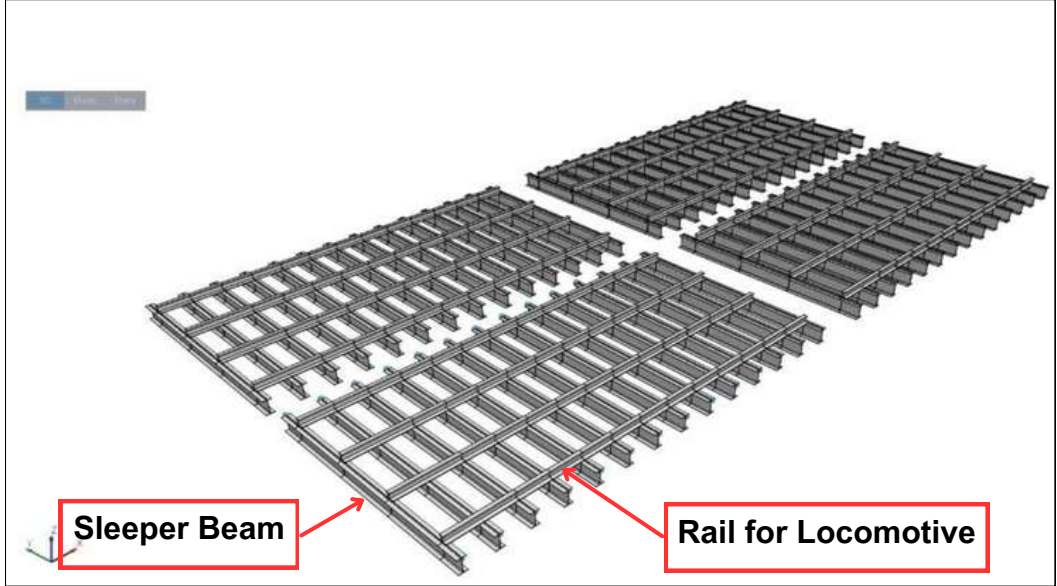
Project : The MRT Purple Line Project Contract 3 Underground Civil Works
Company : Nawarat Patanakarn Public Company Limited
Title : Design Rail Section for Support Locomotive

The purpose of this project is to design rail section with sleeper beam spacing for support locomotive that use for transportation equipment in tunnel.

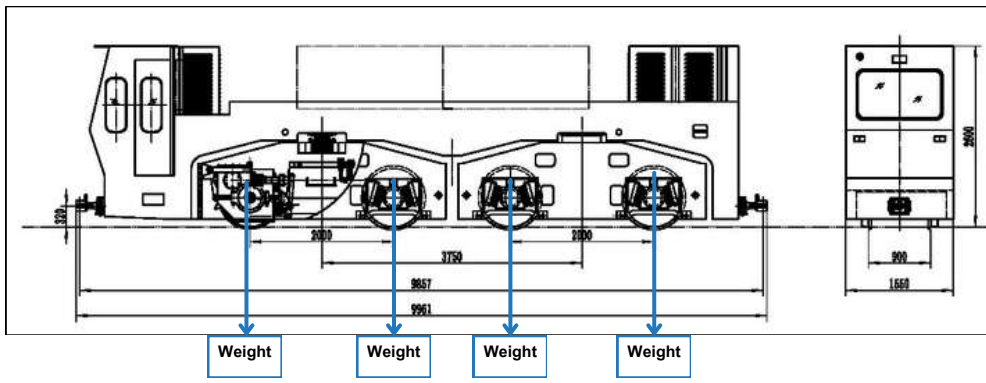
Information for calculation is refer from locomotive specification and rail section property.

Procedure of this project is

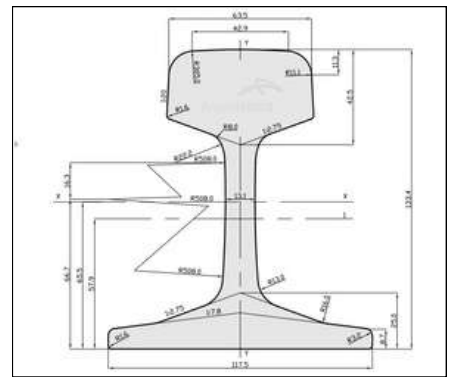
- 1.Design Rail Section by using Microsoft Excel



Structure Model



Locomotive Drawing



Rail Section Drawing

Rail Calculations for Main Drive (45 T Locomotive 8 wheels)

1 Condition

1.1 Spacing :	L	140.00 cm
1.2 1 Wheel Maximum Load :	W	5,625.00 kg
	Number of Wheel	8 wheel
	Total Load	45,000.00 kg
1.3 Tensile Strength :	σ	7,000.00 ksc
1.4 Safety Factor :	SF	6
1.5 Allowable Stress of Rail :	σ allow	1,166.00 ksc
1.6 Elastic Modulus :	E	2,100,000.00 ksc

1.7 Type and Section for Rail Property

Type	Weight (kg/m)	Moment of Inertia : I (cm ⁴)	Section Modulus : Z
15 kg	15.20	167.00	40.80
22 kg	22.30	339.00	69.60
30 kg	30.10	604.00	108.00
37 kg	37	952.00	149.00
39 E1	39.77	1204.90	177.80

2 Calculation

2.1 Required Section Modulus : Z

$$Z_{\text{required}} = \frac{L}{4} \times \frac{W}{\sigma_{\text{allow}}}$$

$$Z_{\text{required}} = \frac{140.00}{4} \times \frac{5,625.00}{1,166.00}$$

$$Z_{\text{required}} = 168.85 \text{ cm}^3$$

2.2 Provided Section

Select Type 39 E1 $Z_{\text{provided}} = 177.80 \text{ cm}^3$ Ok

2.3 Deflection of Rail

$$\delta_{\text{allow}} = 0.39 \text{ cm}$$

$$\delta = \frac{1}{48} \times \frac{W}{E} \times \frac{L^3}{I}$$

$$\delta = \frac{1}{48} \times \frac{5,625.00}{2,100,000.00} \times \frac{2,744,000.00}{1,204.90}$$

$$\delta = 0.127 \text{ cm} \quad \text{Ok}$$

So, Sleeper with spacing 1400 mm with Rail 39 E1 Ok

Calculation Sheet

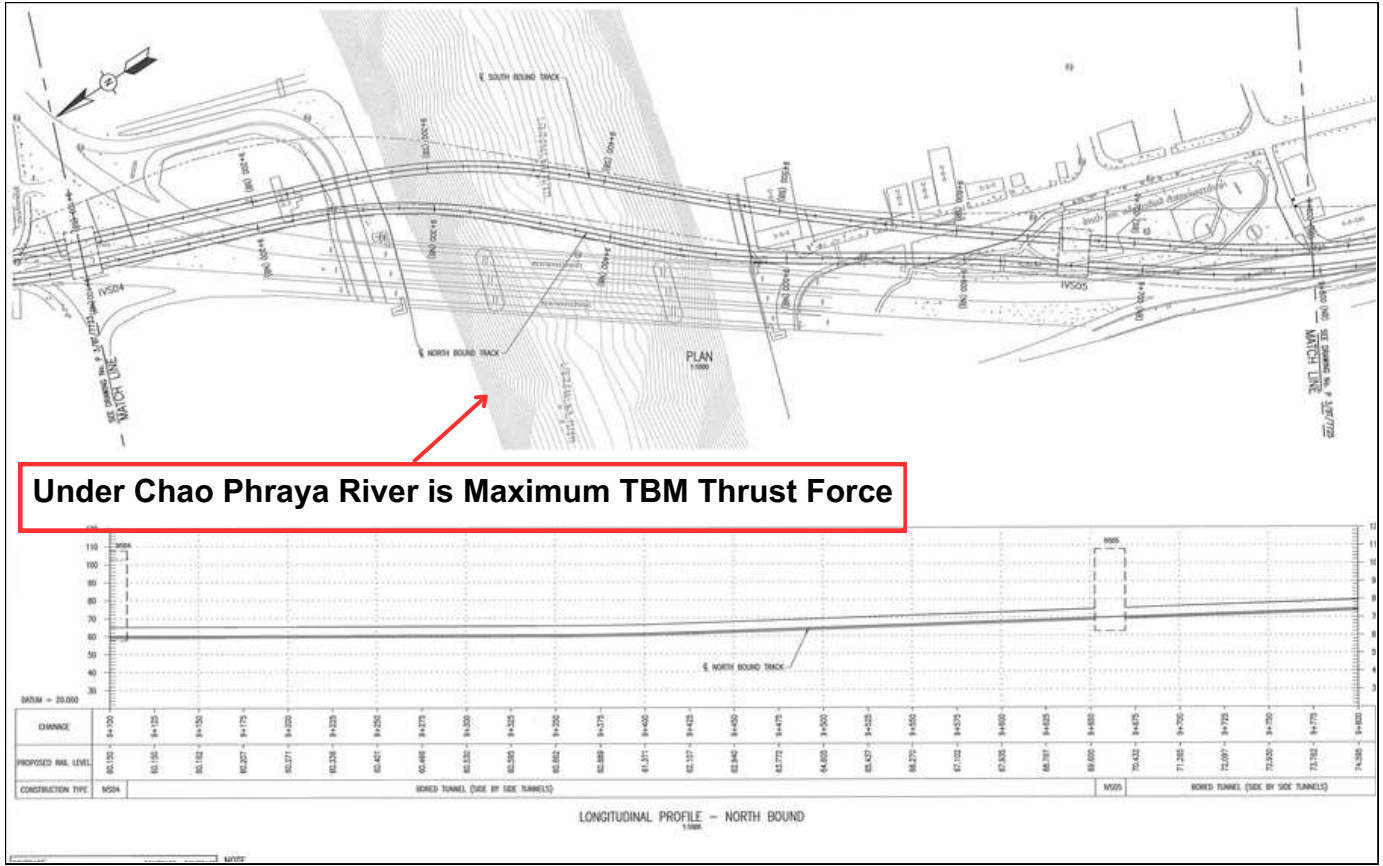
Project : The MRT Purple Line Project Contract 3 Underground Civil Works
Company : Nawarat Patanakarn Public Company Limited
Title : Calculation TBM Thrust Force

The purpose of this project is to evaluate and recheck TBM thrust force with the TBM distributor that consistent with actual situation.

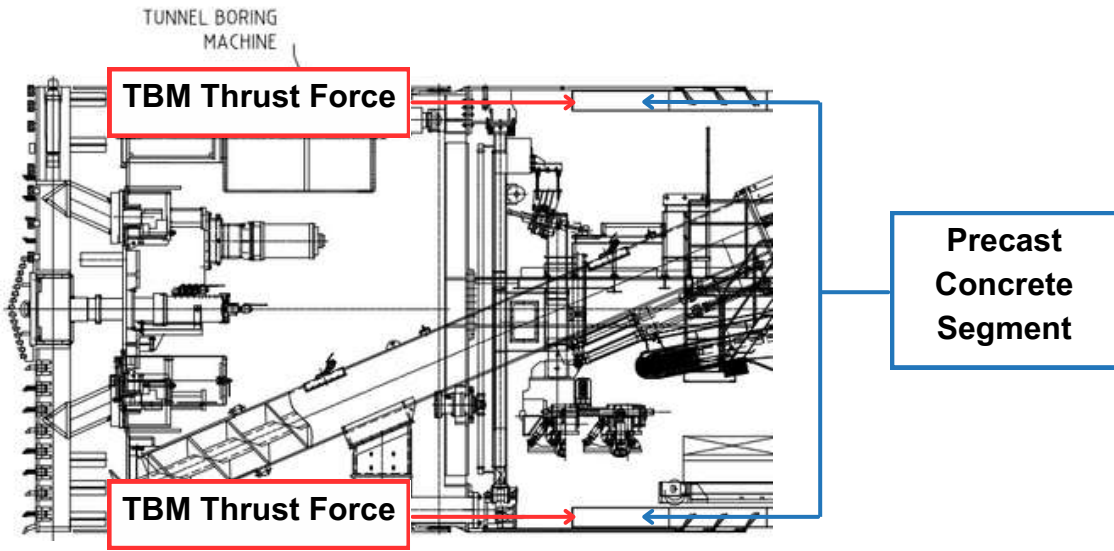
Information for calculation is refer from TBM specification and soil investigation report.

Procedure of this project is

1. Calculation TBM Thrust Force by using Microsoft Excel



Reference Drawing



TBM Drawing

THK-TD-6822053 6.39m EPB TBM DESIGN CALCULATION DOCUMENT (NEW)

Launching Thrust Force Estimation Result

		D-wall Cutting (KN)	Temporary(KN) Ring (T11-T1)	Permanent Ring(KN) (P1 to P100)
Frictional Resistance of Shield Outer Circumference and the Soil	F1(KN)	Shield Frame Remaining inside Shaft	7,824	7,824
Cutting Front Face Resistance	F2(KN)	13,935	13,935	13,935
Frictional Resistance between Tail Frame Plate and Segment	F3(KN)	110	110	110
Traction Resistance of Backup Cars	F4(KN)	0	0	308
Friction of Entrance Seal	F5(KN)	300	300	0
Cutting Friction of Dwall	F6(KN)	1500 (Estimated)	0	0
Friction of Launching Cradle	F7(KN)	100	100	0
Total Required Thrust Force	FXT(KN)	15,945	22,269	22,177

Details of Calculation

F1 7,824 kN (Frictional resistance of shield outer circumference and the soil)

Parameter

Pe	170.71	kN/m ²			
Q1e	85.36	kN/m ²	Pm	134.43	kN/m ² (Average earth pressure working on shield outer diameter)
Q2e	110.92	kN/m ²			
Lm	9665	m	A1	194.0	m ² (Shield machine body surface area)
D0	6.39	m			
	Mu1			0.3	(Friction coefficient between soil and shield)

F2 13,934.8 kN (Cutting front face resistance)

Parameter

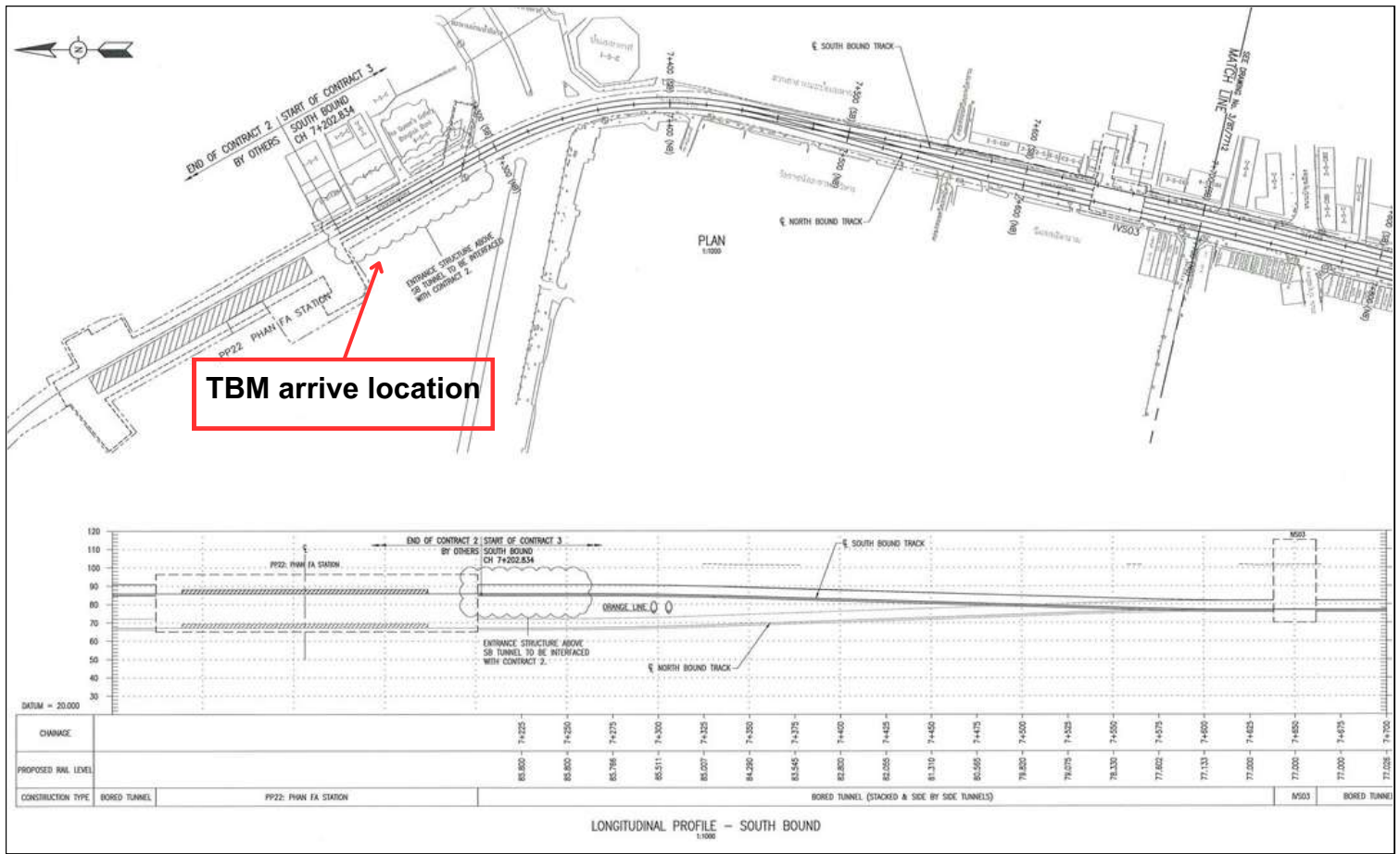
	A0			32.4	m ² (Shield machine excavating area)
Q1	385.36	kN/m ²			
Q2	474.82	kN/m ²	Pf	430.09	kN/m ² (Cutting front face resistance earth pressure)

Calculation Sheet

Project : The MRT Purple Line Project Contract 3 Underground Civil Works
Company : Nawarat Patanakarn Public Company Limited
Title : Calculation Soil Bearing Capacity for TBM

The purpose of this project is to calculate soil bearing capacity when TBM arrive at the location that refer from Terzaghi theory and Meyerhof theory.
 If soil bearing capacity is not enough the company have to do ground improvement.
 Information for calculation is refer from TBM specification and soil investigation report.

Procedure of this project is
 1. Calculation Soil Bearing Capacity by using Microsoft Excel



Reference Drawing

Shallow Foundation for TBM								
Unit weight	2.04	t/m ³	TBM Weight	310.5	t	TMB Dia.	6.39	m
h (from GL)	11.405	m	L	9.665	m	Df	17.795	m
Bearing Pressure	23.2662	t/m ²	B	4.52	m			
			TBM Uniform Load	7.11	t/m ²			
Bearing Pressure above TMB	23.2662	t/m ²						
Bearing Pressure below TBM	30.38	t/m ²	Applied					
Terzaghi Theory							<i>Lf < B</i>	<i>Wrong</i>
Type of Soil	Clay							
C	10.7	t/m ²	ϕ	0	degree			
			Nc	5.70	Nq	1.00	N γ	0.00
qu	97.29	t/m ²						
Factor Safety	3							
qa	32.43	t/m ²	Allowable	OK	Allowable Bearing Pressure > Bearing Pressure			
Meyerhof Theory								
Shape Factors			Depth Factors		Load Inclination Factors		Bearing Capacity Factors	
Sc	1.09	dc	1.79	ic	1.00	Nc	5.14	
Sq	1.05	dq	1.39	iq	1.00	Nq	1.00	
S γ	0.81	d γ	1.00	i γ	1.00	N γ	0.00	
qu	160.47	t/m ²						
Factor Safety	3							
qa	53.49	t/m ²	Allowable	OK	Allowable Bearing Pressure > Bearing Pressure			

* SPT-N Value for estimated cohesion (C)

* Assume Soil until GL Level - below TBM Level is same classification

* Unit weight is maximum value estimate from upper depth sample and below depth sample

Calculation Sheet